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(54) **Modified platinum aluminide diffusion coating and CVD coating method**

Modifizierte Platinaluminid-Diffusionsbeschichtung und CVD-Verfahren

Revêtement par diffusion de platine-aluminure modifié et procédé de dépôt chimique en phase vapeur

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(56) References cited:
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Description**FIELD OF THE INVENTION**

5 [0001] The present invention relates to active element modified platinum aluminide diffusion coatings and chemical vapor deposition (CVD) methods for their manufacture.

BACKGROUND OF THE INVENTION

10 [0002] At temperatures greater than about 1000°C (1832°F), high temperature oxidation is the most important form of environmental attack observed with aluminide diffusion coatings. High temperature oxidation is a chemical reaction whose rate controlling process for an aluminide coating is diffusion through a product (oxide) layer. Diffusion is a thermally activated process, and consequently, the diffusion coefficients are exponential functions of temperature. Since the oxidation of aluminide coatings is a diffusion controlled reaction and diffusion coefficients are exponential
 15 functions of temperature., the oxidation rate is also an exponential function of temperature. At low temperatures where diffusion coefficients are relatively small, the growth rate of a protective scale on any aluminide coating is also small. Thus, adequate oxidation resistance should be provided by any state of the art aluminide coatings, such as: chromium aluminide, aluminide or two phase [PtAl₂ + (Ni,Pt)Al] platinum aluminide, all inward grown coatings made by pack cementation. However, at high temperatures where the diffusion coefficients and consequently the oxidation rate in-
 20 crease rapidly with increasing temperature, only coatings which form high purity alumina (Al₂O₃) scales are likely to provide adequate resistance to environmental degradation.

[0003] The presence of platinum in nickel aluminide has been concluded to provide a number of thermodynamic and kinetic effects which promote the formation of a slow growing, high purity protective alumina scale. Consequently, the high temperature oxidation resistance of platinum modified aluminide diffusion coatings generally is better as compared
 25 to aluminide diffusion coatings not containing platinum.

[0004] In recent years, several limitations of the industry standard, two phase [PtAl₂ + (Ni,Pt)Al], inward grown platinum aluminide coatings have been identified. First, the two phase coatings have metastable phase assemblages and thicknesses, as demonstrated in engine tests at both General Electric and Rolls-Royce. Second, the two phase coatings are sensitive to TMF cracking in engine service, and the growth of these coatings in service only makes this problem
 30 worse. Third, the thick, inward grown platinum aluminides exhibit rumpling during both cyclic oxidation and engine testing. This phenomenon can have undesirable consequences when platinum aluminide coatings are used as the bond coat in thermal barrier coating systems. Fourth, the two phase platinum aluminide coatings are hard and brittle, and this can result in chipping problems during post coat handling and assembly operations.

[0005] Many of the problems encountered with the previous industry standard platinum aluminides can be attributed
 35 to the two phase, inward grown structure and can be overcome by using outwardly grown, single phase platinum aluminide coatings as described, for example, in the Conner et al. technical articles entitled "Evaluation of Simple Aluminide and Platinum Modified Aluminide Coatings on High Pressure Turbine Blades after Factory Engine testing", Proc. AMSE Int. Conf. of Gas Turbines and Aero Engine Congress June 3-6, 1991 and June 1-4, 1992. For example, the outwardly grown, single phase coating microstructure on directionally solidified (DS) Hf-bearing nickel base super-
 40 alloy substrates was relatively unchanged after factory engine service in contrast to the microstructure of the previous industry standard two phase coatings. Further, the growth of a CVD single phase platinum aluminide coating was relatively insignificant compared to two phase coatings during factory engine service. Moreover, the "high temperature low activity" outward grown platinum aluminide coatings were observed to be more ductile than inward grown "low temperature high activity" platinum aluminide coatings.

45 [0006] WO-A-96/13622 in the name of the inventors of the present invention described a CVD process for making a single phase outwardly grown platinum aluminide diffusion coating on a nickel base superalloy substrate, such as IN 738.

[0007] Copending applications Serial Nos. 08/197 478 and 08/197 497 also of common assignee disclose CVD methods for codeposition of aluminum, silicon and one or more active elements, such as yttrium, hafnium and/or zir-
 50 conium, on a substrate to form a platinum aluminide diffusion coating modified by the inclusion of the active element(s).

[0008] WO-A-96/15284 discloses a method of producing a reactive element modified aluminide diffusion coating on a metal substrate comprising the step of depositing a metal coating including at least one reactive element on a metal substrate.

55 **SUMMARY OF THE INVENTION**

[0009] The present invention provides a CVD outwardly grown platinum aluminide diffusion coating on a nickel or cobalt base superalloy substrate wherein the platinum modified aluminide diffusion coating is modified to include silicon,

hafnium, and optionally zirconium and/or other active elements (e.g. CE, La, Y) each in a concentration of about 0.01 weight % to about 8 weight % of the outer additive layer of the coating. A preferred coating of the present invention includes about 0.01 weight % to less than 2 weight % of each of silicon, hafnium, and optionally zirconium and/or other active elements in the outer additive layer, preferably with a Hf/Si ratio less than about 1 and, when Zr also is present, a Hf+ Zr/Si ratio of less than about 1. A coating microstructure is provided characterized by an inner diffusion zone or region adjacent the substrate and the outer additive layer having a single (Ni, Pt)(Al, Si) matrix phase including hafnium silicide and other silicide second phase particles or regions dispersed throughout the matrix phase of the additive layer. Carbide particles may also be present.

[0010] The present invention also provides a thermal barrier coating system including the aforementioned CVD outwardly grown active element modified platinum aluminide diffusion coating as an intermediate bond coat between a nickel or cobalt base superalloy substrate and an outer ceramic thermal barrier layer, such as an physical vapor deposited (PVD) columnar ceramic layer deposited on a thin alumina layer formed on the bond coat.

[0011] A method of making such CVD active element modified platinum aluminide diffusion coatings on nickel or cobalt base superalloy substrates is described wherein in one embodiment a platinum layer first is deposited on the substrate followed by CVD codeposition of Al+Si+Hf+optionally Zr and/or other active elements to produce a diffusion coating useful, although not limited, for service applications in the hot turbine section of a gas turbine aircraft engine where shorter overhaul intervals are practiced.

[0012] Another method involves first CVD codepositing Al+Si+Hf+optionally Zr and/or other active elements on the substrate to form an initial active element bearing aluminide diffusion layer, then depositing platinum on the layer, and finally CVD aluminizing the Pt coated initial layer to produce a thicker overall aluminide diffusion coating useful, although not limited, for service applications where longer overhaul intervals can be tolerated, such as land based gas turbine engines.

DESCRIPTION OF THE DRAWINGS

[0013] Figure 1 is a graph depicting comparative cyclic oxidation resistance at 1093°C (2000 degrees F) of a conventional aluminide coating, such as an inwardly grown platinum aluminide coating designated LDC-2E and an inwardly grown CVD platinum aluminide MDC-150, an outwardly grown single phase CVD platinum aluminide diffusion coating designated MDC-150L, and coatings in accordance with the present invention designated MDC-151L and MDC-152L, all coatings being formed on substrates of conventional IN 738 nickel base superalloy.

[0014] Figure 2 is a graph depicting comparative cyclic oxidation resistance at 1177°C (2150 degrees F) of coatings in accordance with the present invention designated MDC-151L and MDC-152L at different Hf/Si ratios, all coatings being formed on substrates of conventional RENE' N5 nickel base superalloy.

[0015] Figures 3A, 3B are photomicrographs at 1000X of the microstructure of a representative coating of the present invention designated MDC-151L on respective substrates as coated of conventional PWA 1480 and Rene' N5 nickel superalloys.

[0016] Figure 4 is a photomicrograph at 500X of the microstructure of a representative coating of the present invention designated MDC-151L on PWA 1480 nickel superalloy substrate after exposure at 2150 degrees F for 250 hours.

[0017] Figure 5 is a photomicrograph at 250X of the microstructure of a representative thermal barrier coating of the present invention designated MDC-152L on Rene' N5 nickel superalloy substrate.

DETAILED DESCRIPTION

[0018] The present invention provides a CVD outwardly grown active element modified platinum aluminide diffusion coating on a nickel or cobalt base superalloy substrate, especially a single crystal superalloy substrate, to substantially improve oxidation resistance at elevated temperatures.

[0019] Chemical vapor deposition (CVD) is a process which is used for the transport of aluminum and one or more active elements as halide gases from a low temperature metal halide generator to a substrate, such as a high pressure nickel or cobalt superalloy turbine component, positioned inside a high temperature reactor. In the practice of the present invention, a CVD process can be advantageously employed to form the outwardly grown active element modified platinum aluminide diffusion coating on a nickel or cobalt base superalloy substrate. That CVD process involves exposure of the superalloy substrate at an elevated substrate coating temperature of at least 1000 degrees C in the coating reactor or retort to a high purity coating gas comprising a mixture of hydrogen and aluminum trichloride gases and others in a manner that decreases the concentration of substitutional alloying elements, such as refractory elements present in the substrate (e.g. Ta, W, Mo, Ti, Re, etc.), and surface active solute elements, such as S, P, B, in an outwardly grown platinum aluminide diffusion coating, further details of that CVD process being available in WO-A-96/13622.

[0020] The CVD outwardly grown active element modified platinum aluminide diffusion coating in accordance with the present invention is modified to include silicon, hafnium, and optionally zirconium and/or other active elements,

such as Ce, La, Y, etc., each in a concentration of about 0.01 weight % to 8 weight % of the outer additive portion of the coating represented by (Ni,Pt)(Al,Si), see Figures 3A, 3B showing the outer additive layer and the inner diffusion zone or layer adjacent the substrate of the coating as-coated. Preferably, the concentration of the hafnium and zirconium and/or other active elements, if present, is maximum at approximately 2 weight % in the region of the additive layer adjacent the diffusion zone and decreases toward the outer surface of the additive layer to a trace concentration. The concentration of the silicon is within the above range generally uniformly through the additive layer. The concentration of the platinum is a maximum of approximately 35 weight % near the outer surface of the additive layer and decreases toward the diffusion zone to a lower concentration near the diffusion zone; e.g. as low as 5 weight % or less.

[0021] The overall Pt concentration in the additive layer of the coating is 10 to 30 weight %. The overall Al concentrations of the additive layer are 10 to 30 weight % Al. The diffusion zone includes mostly refractory elements as intermetallic or carbide phases.

[0022] A preferred coating of the present invention in as-coated condition includes about 0.01 weight % to less than 2 weight % of each of silicon, hafnium, and optionally zirconium and/or other active elements preferably with a Hf/Si ratio less than about 1 and, when Zr also is present, a Hf+ Zr/Si ratio of less than about 1. A more preferred coating as-coated includes from about 0.25 to about 0.75 weight % Si and about 0.075 to about 0.125 weight % Hf. A particular coating includes 0.5 weight % Si and 0.1 weight % Hf in the as-coated condition.

[0023] The CVD outwardly grown active element modified platinum aluminide diffusion coating in accordance with the present invention includes a coating microstructure characterized by an inner diffusion zone or layer adjacent the substrate and a (Ni,Pt)(Al,Si) outer additive layer, Figures 3A, 3B. Importantly, the outer additive layer includes second phase particles or regions (shown as the light particles or regions in Figure 3A, 3B) comprising primarily hafnium silicides with some zirconium silicide and hafnium + zirconium silicides present preferably present as spheres or needles dispersed throughout the outer additive layer of the coating. Other particles or regions also may be present in the additive layer in the as-coated condition and may include carbides of hafnium, zirconium and hafnium + zirconium formed by reaction with carbon in the substrate alloy.

[0024] The CVD outwardly grown active element modified platinum aluminide diffusion coating in accordance with the present invention exhibits substantially improved high temperature oxidation resistance as illustrated in Figure 1 wherein Figure 1 is a graph depicting comparative cyclic oxidation resistance at 1093°C (2000 degrees F) of a conventional aluminide coating, such as an inwardly grown platinum aluminide coating designated LDC-2E and MDC-150, an outwardly grown single phase platinum aluminide diffusion coating designated MDC-150L, and coatings in accordance with the present invention designated MDC-151L and MDC152L, all coatings being formed on IN 738 nickel base superalloy substrates in the form of test tabs having dimensions of 3.175 mm (1/8 inch) by 12.7 mm (1/2 inch) by 25.4 mm (1 inch).

[0025] The coating parameters for each coating formed are set forth herebelow:

[0026] The predominantly inwardly grown LDC-2E platinum aluminide coating was formed at a substrate temperature of 982 degrees C using a pack composition comprising 33 % by weight alloy powder (56 weight % Cr and 44 weight % Al) and balance alumina. The substrate was first electroplated with Pt (9-11 mg/cm²) and diffused into the substrate by heat treatment at a temperature of 1052 degrees C for 1 hour prior to pack cementation. Pt was electroplated from a plating bath based upon a HPO₄/H₂PO₄ buffer at a current density of 0.09 amperes per square centimeters pursuant to US Patents 3 677 789 and 3 819 338.

[0027] The inwardly grown CVD platinum modified aluminide coating MDC-150 was formed at a substrate temperature of 1010 °C using coating gas mixture comprising 12 volume % aluminum chlorides (AlCl₃, AlCl₂ and AlCl) and 88 volume % hydrogen. The coating gas mixture was generated by passing hydrogen and hydrogen chloride in mixture of hydrogen/12 volume % HCl over a 99.999 % pure external source of aluminum at 290 °C and then passing the mixture through a high temperature generator in the coating retort at 1010 degrees C to form a mixture of aluminum trichlorides and subchlorides. The substrate was first electroplated with Pt (9-11 mg/cm²) as described above and diffused into the substrate by heat treatment at a temperature of 926 degrees C for 2 hours prior to CVD aluminizing.

[0028] The outwardly grown CVD single phase platinum aluminide coating MDC-150L was formed at a substrate temperature of 1080 °C using coating gas mixture comprising 5.5 volume % aluminum trichloride, 94.5 volume % hydrogen at a flow rate of 230 scfh in calculation of volume %'s. The coating gas mixture was generated by passing high purity hydrogen (e.g. less than 30 ppb impurities) and high purity hydrogen chloride (e.g. less than 25 ppm impurities) in mixture of hydrogen/15 volume % HCl over a high purity 99.999 % pure external source of aluminum at 290 °C. The HCl which produced the purification of the substrate and coating was produced by the hydrogen reduction of aluminum trichloride on the sample surface. The substrate was first electroplated with Pt (9-11 mg/cm²) as described above without a prediffusion heat treatment prior to CVD aluminizing.

[0029] The active element modified platinum aluminide diffusion coating MDC-151L of the present invention was formed pursuant to a two step method of the invention involving depositing platinum on the substrate and then CVD codepositing Al+Si+Hf+optionally Zr on the Pt layer to form a active element bearing platinum aluminide diffusion coating. CVD apparatus of the type shown in US Patent 5,261,963 can be employed. The substrate first was electro-

plated with Pt (9-11 mg/cm²) as described above without any diffusion heat treatment of the platinum layer prior to CVD codeposition. Higher Pt amounts can be deposited, if desired, to further improve oxidation resistance of the coating. Electroplating of the platinum layer alternately can be achieved using an aqueous potassium hydroxide solution having greater than about 9 grams per liter potassium hydroxide having less than 5 parts per million sulfur and phosphorus and about 10-11 grams platinum per liter added to solution as hexahydroxy platinic acid having less than 5 parts per million sulfur and phosphorous and less than 10 parts per million chlorine at a solution temperature of about 70 degrees C and pH of greater than 11.2 and less than 11.9 and electrical current density less than 0.020 ampere/cm² (e.g. 0.015 ampere/cm²) as described in copending application in the name of one inventors, EP-A-0 821 075, corresponding to US-A-5,788,823 entitled "Platinum Modified Aluminide Diffusion Coating And Method". The second step was conducted at a substrate temperature of 1080 °C using coating gas mixture comprising 4 volume % silicon tetrachloride and aluminum trichloride (greater than 90% by volume aluminum trichloride), 79.5 volume % hydrogen, 15 volume % Ar, and 1.5 volume % HfCl₄ and ZrCl₄ [(coating gas flow rate of 1.57 liter per second [200 standard cubic feet per hour (scfh)] and total pressure of 2·10⁴ Pascal (150 Torr)]. The coating gas mixture was generated by passing high purity hydrogen (e.g. less than 30 ppb impurities) and high purity hydrogen chloride (e.g. less than 25 ppm impurities) in mixture of hydrogen/10 volume % HCl over a high purity 99.999 % pure source of aluminum and then passing the mixture over a high purity 99.999 % pure source of silicon with both sources at 290 degrees C (sources external of retort) to form a mixture of aluminum trichloride and silicon tetrachloride. A mixture of Ar/10 volume % HCl was flowed in an external chloride generator through a hafnium bed at 430 °C to form hafnium tetrachloride containing a small amount (e.g. less than 1 volume %) of zirconium tetrachloride. The hafnium bed included a small concentration of zirconium, such as less than 1 weight % Zr. Alternately, the coating gas mixture can be flowed through a cogenerator having a hafnium bed and a zirconium bed downstream of the hafnium bed to form coating gas mixture. The gas mixtures were introduced concurrently to the coating retort to codeposit Al+Si+Hf+Zr on the IN 738 substrate. The HCl which produced the purification of the substrate and coating was produced by the hydrogen reduction of the various metal chloride gases on the sample surface.

[0030] The active element modified platinum aluminide diffusion coating MDC-152L of the present invention was formed pursuant to a three step method of the invention involving first CVD codepositing Al+Si+Hf+optionally Zr on the substrate to form an initial active element bearing aluminide diffusion layer, then depositing platinum on the layer, and finally CVD aluminizing the Pt coated initial layer to produce a thicker overall aluminide diffusion coating useful, although not limited, for service applications where longer overhaul intervals can be tolerated, such as land based gas turbine engines. CVD apparatus of the type shown in US Patent 5,261,963 can be employed. The first step was conducted at a substrate temperature of 1080 °C using coating gas mixture comprising 3.4 volume % aluminum trichloride and silicon tetrachloride (greater than 90% by volume aluminum trichloride), 82.6 volume % hydrogen, 12.7 volume % Ar, and 1.3 volume % HfCl₄ and ZrCl₄ (gas flow rate of 1.86 l/s (236 scfh) and total pressure of 2·10⁴ Pa (150 Torr)). The coating gas mixture was generated by passing high purity hydrogen (e.g. less than 30 ppb impurities) and high purity hydrogen chloride (e.g. less than 25 ppm impurities) in mixture of hydrogen/10 volume % HCl over a high purity 99.999 % pure external source of aluminum and then passing the mixture over a high purity 99.999 % pure external source of silicon both sources at 290 degrees C to form a mixture of aluminum trichloride and silicon tetrachloride. A mixture of Ar/10 volume % HCl was flowed in an external chloride generator through a hafnium bed at 430 °C to form hafnium tetrachloride containing a small amount (e.g. less than 1 volume %) of zirconium tetrachloride. The hafnium bed included a small concentration of zirconium, such as less than 1.0 weight % Zr. The gas mixtures were introduced concurrently to the coating retort to codeposit Al+Si+Hf+Zr on the IN738 substrate. The HCl which produced the purification of the substrate and coating was produced by the hydrogen reduction of the various metal chloride gases on the sample surface. The substrate then was electroplated with Pt (9-11 mg/cm²) as described above without any diffusion heat treatment of the platinum layer prior to the third step. The third step was conducted at a substrate temperature of 1080 °C using coating gas mixture comprising 5.5 volume % aluminum trichloride, 94.5 volume % hydrogen (gas flow rate of 1.73 l/s (220 scfh) and total pressure of 2·10⁴ Pa (150 Torr)). The coating gas mixture was generated by passing high purity hydrogen (e.g. less than 30 ppb impurities) and high purity hydrogen chloride (e.g. less than 25 ppm impurities) in mixture of hydrogen/15 volume % HCl over a high purity 99.999 % pure source of aluminum external of the retort at 290 degrees C.

[0031] In the production of the MDC-150L, MDC-151L, and MDC-152L using the aforementioned CVD coating parameters, the concentrations of substitutional alloying elements, such as Cr, W, Mo, Ta, Fe and others, and surface active solute elements, such as S, P, B in the aluminide diffusion coating are significantly reduced as compared to their corresponding concentrations in the IN738 substrate by the purification effects of the CVD parameters as described in WO-A-96/13622. The removal of these elements during the CVD process involves the chlorination of the metal and subsequent evaporation of the metal chlorides. Note ppb = parts per billion and ppm = parts per million in above description.

EXAMPLES OF CYCLIC OXIDATION TESTING OF PLATINUM ALUMINIDES

[0032] The evaluation of the aforementioned coatings for cyclic oxidation testing involved first examining coating structure and thickness to be tested. The following paragraphs summarize the results of the metallographic and electron microprobe analysis of these coatings in the as-coated condition.

COATING STRUCTURE AND THICKNESS

[0033] In the as-coated condition, both the LDC-2E coating and MDC-150 coating exhibited a two phase outer layer on top of an (Ni,Pt)Al layer and finally a thin diffusion zone. This structure is typical of the present industry standard platinum aluminides. The MDC-150L coating exhibited a single phase (Ni,Pt)Al additive layer and about one third of the thickness was diffusion zone. The MDC-151L and MDC-152L coatings both exhibited an outer additive layer having single (Ni,Pt)(Al,Si) matrix phase including primarily hafnium silicide particles (lighter phase) with some zirconium silicide and possibly some hafnium + zirconium silicides dispersed throughout the matrix phase of the additive layer, similar to Figure 3, and about one third of the thickness was diffusion zone adjacent the substrate. A well developed diffusion zone is characteristic of a growth process dominated by the outward transport of nickel.

[0034] In the as coated condition, the coating thicknesses were as follows: LDC-2E coating = $4.98 \cdot 10^{-2}$ mm (1.96 mils), MDC-150 coating = $5.36 \cdot 10^{-2}$ mm (2.11 mils), MDC-150L coating = $7.95 \cdot 10^{-2}$ mm (3.13 mils), MDC-151L coating = $8.63 \cdot 10^{-2}$ mm (3.4 mils), and MDC-152L coating = $1.30 \cdot 10^{-1}$ mm (5.1 mils).

[0035] After solution heat treatment at 2050 °F for 120 minutes, both the LDC-2E and MDC-150 two phase coatings exhibited significant changes in structure, composition and thickness. The average Pt and Al concentrations decreased significantly, and the thicknesses increased about 52% and 67% for LDC-2E coating and MDC-150 coating, respectively. The MDC-150L coating was single phase and remained relatively unaffected. The microstructure of the MDC-151L and MDC-152L coatings did not change significantly after heat treatment, and these coatings had a single phase matrix with active element rich second phase particles, such as primarily hafnium silicide particles with some zirconium silicide and possibly some hafnium + zirconium silicides, following the heat treatment. It should be noted that the observed metamorphoses of the two phase LDC-2E coating and MDC-150 coatings during the solution heat treatment is similar to the changes encountered during engine testing.

CYCLIC OXIDATION TEST RESULTS

[0036] The IN-738 test tabs with the the different platinum aluminide coatings were used for cyclic oxidation testing at 1093°C (2000° F). A one hour cycle included: fifty minutes at temperature and ten minutes cooling to room temperature. Samples were weighed to the nearest 0.1 milligram (mg) before the test and after each fifty cycle test interval.

[0037] Failure was defined as a negative 0.5 mg/cm² weight loss; that is, when the sample weight after a test interval was -0.5 mg/cm² less than the initial weight. For each coating, three samples were tested to failure, and then the cycles to failure were averaged.

[0038] The results of the testing are summarized in Figure 1 and the Table below, which are based on three (3) samples tested for each type of coating.

TABLE

2000°F CYCLIC OXIDATION OF COATED IN-738		
COATING	ONE HOUR CYCLES TO FAILURE	RELATIVE LIFE
LDC-2E	1350	1
MDC-150	1700	1.26
MDC-150L	1900	1.41
MDC-151L	3475	2.57
MDC-152L	7000	5.19

A comparison of the test results for the platinum modified aluminide coatings shows that the coatings MDC-151L and MDC-152L pursuant to the invention exhibited a substantial (e.g. 2 or more times) increase in relative life in the oxidation test as compared to the LDC-2E coating, MDC-150 coating, and MDC-150L coating. The superior oxidation resistance of the MDC-151L coating and MDC-152L coating compared to the others results from the purification effects produced by the particular CVD aluminizing parameters set forth above and also the presence of the active elements Hf and optional Zr. For example, the effect of the presence of the active elements is evident by comparing the MDC-151L coating and MDC-152L coating versus the MDC-150L coating devoid of active elements. The longer life of the MDC-

152L coating relative to the MDC-151L coating in Figure 1 is due to the greater thickness of the former relative to the latter since the MDC-151L and MDC-152L coatings are generally equal in oxidation resistance on a per mil (0.0254 mm) of coating thickness basis, where Hf/Si ratio is the same for the coatings.

[0039] Based on the test results set forth in Figure 1 and the Table, the CVD outward grown, active element modified platinum aluminide diffusion coatings of the invention represent a significant advancement in platinum modified aluminide coating technology.

[0040] A coating of the present invention includes an outer additive layer having hafnium and silicon in a preferred concentration ratio of less than about 1. When Zr also is present, the concentration ratio Hf+Zr/Si is less than about 1. Referring to Figure 2, normalized cyclic oxidation life at 1177°C (2150 degrees F) versus the Hf/Si concentration ratio is plotted for samples designated MDC-151L and MDC-152L coatings made in the same manner as described hereabove. Sample failure was defined as a weight loss of -5 mg/cm² relative to the initial sample weight. The plot illustrates that the oxidation resistance of the coatings of the invention decreases by 60% as the Hf/Si ratio increases from a small fraction toward 2. This data was used to establish the preferred concentration Hf/Si ratio of less than about 1, or Hf+Zr/Si ratio of less than about 1 when Zr is present since Zr and Hf similarly affect coating behavior.

[0041] Using the CVD codeposition processes described hereabove for the MDC-151L and MDC-152L coatings, the distribution and morphology of hafnium silicide second phase particles can be changed within the preferred coatings of the invention wherein Hf/Si or Hf+Zr/Si is less than about 1. These changes can be effected by changing the HCl flow rate to the active element halide generators and/or cogenerators during the CVD codeposition of the coating.

[0042] A uniform distribution of small hafnium silicide second phase particles as spherulids (e.g. diameter approximately 1 to 5 μm (microns) or needles (e.g. approximately 1 to 5 μm (microns) length and approximately 0.5 to 1 μm (micron) thickness) in the single matrix phase of the outer additive layer is preferred for high temperature oxidation resistance. However, other distributions of the second phase particles may be used.

[0043] The active element modified platinum aluminide diffusion coating of the present invention is useful in thermal barrier coating systems wherein the CVD outwardly grown active element modified platinum aluminide diffusion coating is present as an intermediate bond coat between a nickel or cobalt base superalloy substrate and an outer ceramic thermal barrier layer, such as an physical vapor deposited (PVD) columnar ceramic layer deposited on a thin alumina layer formed on the bond coat. Referring to Figure 3A, 3B, a MDC-151L coating of the present invention is shown on respective PWA 1480 and Rene' N5 substrates and includes acicular hafnium silicide particles (light colored particles) near the outer and inner surface of the outer additive layer of the coating in addition to being present at other regions of the additive layer. The presence of acicular second phase particles near the outer surface of the coating in Figure 3A is possible with the MDC-151L coating of the invention. Referring to Figure 4, a MDC-151L coating on the PWA 1480 substrate after an exposure of 250 hours to cyclic oxidation at 1177°C (2150 degrees F) is shown. The presence of hafnium rich stringers at the outer surface of the coating is observed and may improve bonding of the ceramic thermal barrier layer, Figure 5, to the aluminide diffusion coating (MDC-152L shown in Figure 5).

Claims

1. Chemical vapor deposited outwardly grown platinum aluminide diffusion coating on a nickel or cobalt base superalloy substrate wherein the platinum aluminide diffusion coating has a microstructure comprising an inner diffusion zone adjacent the substrate and an outer additive layer, said outer layer consisting essentially of platinum, aluminum, nickel, silicon and hafnium, **characterized in that** silicon is present in a concentration of 0.01 weight % to 8 weight %, that hafnium is present in a concentration of 0.01 weight % to 8 weight %, that said outer additive layer includes a single phase matrix with second phase particles dispersed therein, and that said second phase particles comprise hafnium silicides.
2. The coating of claim 1 wherein the coating includes about 0.01 weight % to less than 2 weight % of each of silicon, hafnium, and at least one of zirconium and an active element selected from the group consisting of Ce, La, Y, Mg, and Ca in the outer additive layer.
3. The coating of claim 1 or 2 having a Hf/Si ratio less than about 1.
4. The coating of claim 1 or 2 having a Hf+ Zr/Si ratio of less than about 1 when Zr is present.
5. The coating of one of the preceding claims wherein the second phase particles are present as spheres or needles dispersed throughout the outer additive layer of the coating.
6. The coating of one of the preceding claims wherein acicular second phase particles comprising hafnium silicide

are present at the outer surface of the coating.

7. A thermal barrier coating system including a nickel or cobalt base superalloy substrate, a chemical vapor deposited outwardly grown platinum aluminide diffusion coating on the nickel or cobalt base superalloy substrate wherein the platinum aluminide diffusion coating has a microstructure comprising an inner diffusion zone adjacent the substrate and an outer additive layer, said outer layer consisting essentially of platinum, aluminum, nickel, silicon and hafnium, **characterized in that** silicon is present in a concentration of 0.01 weight % to 8 weight %, that hafnium is present in a concentration of about 0.01 weight % to 8 weight %, that said outer additive layer includes a single phase matrix with second phase particles dispersed therein, that said second phase particles comprise hafnium silicides and that said coating system includes a ceramic layer on the aluminide diffusion coating.
8. The coating system of claim 7 wherein the aluminide diffusion coating includes about 0.01 weight % to less than 2 weight % of each of silicon, hafnium, and at least one of zirconium and an active element selected from the group consisting of Ce, La, Y, Mg, Ca in the outer additive layer.
9. The coating system of claim 7 or 8 wherein the aluminide diffusion coating includes a Hf/Si ratio less than about 1.
10. The coating system of claim 7 or 8 wherein the aluminide diffusion coating includes a Hf+Zr/Si ratio less than about 1.
11. The coating system of one of claims 7 to 10 wherein acicular hafnium silicide second phase particles are present at the outer surface of the coating.

Patentansprüche

1. Durch einen Prozess der chemischen Abscheidung aus der Gasphase niedergeschlagene, nach außen gewachsene Platinaluminid-Diffusionsbeschichtung auf einem Nickel- oder Cobaltbasis-Superlegierungssubstrat, wobei die Platinaluminid-Diffusionsbeschichtung eine Mikrostruktur aufweist, welche eine innere Diffusionszone benachbart zu dem Substrat und eine äußere Additivschicht aufweist, wobei die äußere Schicht im Wesentlichen aus Platin, Aluminium, Nickel, Silicium und Hafnium besteht, **dadurch gekennzeichnet, dass** Silicium in einer Konzentration von 0,01 Gew.-% bis 8 Gew.-% vorliegt, dass Hafnium in einer Konzentration von 0,01 Gew.-% bis 8 Gew.-% vorliegt, dass die äußere Additivschicht eine Einphasen-Matrix mit darin dispergierten Zweitphasenpartikeln aufweist und dass die Zweitphasenpartikel Hafniumsilicide umfassen.
2. Beschichtung nach Anspruch 1, wobei die Beschichtung jeweils ca. 0,01 Gew.-% bis weniger als 2 Gew.-% Silicium, Hafnium und mindestens eines der Elemente, welche sind Zirkonium und ein aus der aus Ce, La, Y, Mg und Ca bestehenden Gruppe ausgewähltes aktives Element, in der äußeren Additivschicht enthält.
3. Beschichtung nach Anspruch 1 oder 2 mit einem Hf/Si-Verhältnis von kleiner als ca. 1.
4. Beschichtung nach Anspruch 1 oder 2 mit einem Hf+Zr/Si-Verhältnis von kleiner als ca. 1 bei Vorhandensein von Zr.
5. Beschichtung nach einem der voranstehenden Ansprüche, wobei die Zweitphasenpartikel als in der gesamten äußeren Additivschicht der Beschichtung dispergierte Kugeln oder Nadeln vorliegen.
6. Beschichtung nach einem der voranstehenden Ansprüche, wobei azikuläre Zweitphasenpartikel, welche Hafniumsilicid umfassen, an der äußeren Oberfläche der Beschichtung vorliegen.
7. Wärmebarriere-Beschichtungssystem mit einem Nickel- oder Cobaltbasis-Superlegierungssubstrat, einer durch einen Prozess der chemischen Abscheidung aus der Gasphase niedergeschlagenen, nach außen gewachsenen Platinaluminid-Diffusionsbeschichtung auf dem Nickeloder Cobaltbasis-Superlegierungssubstrat, wobei die Platinaluminid-Diffusionsbeschichtung eine Mikrostruktur aufweist, welche eine innere Diffusionszone benachbart zu dem Substrat und eine äußere Additivschicht aufweist, wobei die äußere Schicht im Wesentlichen aus Platin, Aluminium, Nickel, Silicium und Hafnium besteht, **dadurch gekennzeichnet, dass** Silicium in einer Konzentration von 0,01 Gew.-% bis 8 Gew.-% vorliegt, dass Hafnium in einer Konzentration von ca. 0,01 Gew.-% bis 8 Gew.-% vorliegt, dass die äußere Additivschicht eine Einphasen-Matrix mit darin dispergierten Zweitphasenpartikeln aufweist, dass die Zweitphasenpartikel Hafniumsilicide umfassen und dass das Beschichtungssystem eine Keramik-

schicht auf der Aluminid-Diffusionsbeschichtung aufweist.

- 5 8. Beschichtungssystem nach Anspruch 7, wobei die Aluminid-Diffusionsbeschichtung jeweils ca. 0,01 Gew.-% bis weniger als 2 Gew.-% Silicium, Hafnium und mindestens eines der Elemente, welche sind Zirkonium und ein aus der aus Ce, La, Y, Mg, Ca bestehenden Gruppe ausgewähltes aktives Element, in der äußeren Additivschicht enthält.
- 10 9. Beschichtungssystem nach Anspruch 7 oder 8, wobei die Aluminid-Diffusionsbeschichtung ein Hf/Si-Verhältnis von kleiner als ca. 1 aufweist.
- 10 10. Beschichtungssystem nach Anspruch 7 oder 8, wobei die Aluminid-Diffusionsbeschichtung ein Hf+Zr/Si-Verhältnis von kleiner als ca. 1 aufweist.
- 15 11. Beschichtungssystem nach einem der Ansprüche 7 bis 10, wobei azikuläre Hafniumsilicid-Zweitphasenpartikel an der äußeren Oberfläche der Beschichtung vorliegen.

Revendications

- 20 1. Revêtement par diffusion de platine-aluminure croissant vers l'extérieur, déposé par dépôt chimique en phase vapeur, sur un substrat en super-alliage à base de cobalt ou de nickel, dans lequel le revêtement par diffusion de platine-aluminure a une microstructure comprenant une zone de diffusion intérieure, adjacente au substrat, et une couche d'additif extérieure, ladite couche extérieure se composant essentiellement de platine, d'aluminium, de nickel, de silicium et d'hafnium, **caractérisé en ce que** le silicium est présent en une concentration comprise entre 25 0,01 % en poids et 8 % en poids, **en ce que** l'hafnium est présent en une concentration comprise entre 0,01 % en poids et 8 % en poids, **en ce que** ladite couche d'additif extérieure comprend une matrice à phase unique comportant des particules dispersées dans celle-ci, formant une seconde phase, et **en ce que** lesdites particules de la seconde phase comprennent des siliciures d'hafnium.
- 30 2. Revêtement selon la revendication 1 dans lequel le revêtement comprend entre environ 0,01 % et moins de 2 % en poids de silicium, d'hafnium et d'au moins un élément qui est du zirkonium ou un élément actif sélectionné dans le groupe consistant en Ce, La, Y, Mg et Ca dans la couche d'additif extérieure.
- 35 3. Revêtement selon la revendication 1 ou 2 ayant un rapport Hf/Si inférieur à environ 1.
- 40 4. Revêtement selon la revendication 1 ou 2 ayant un rapport Hf + Zr/Si inférieur à environ 1 quand Zr est présent.
5. Revêtement selon l'une des revendications précédentes dans lequel les particules de la seconde phase sont présentes sous forme de sphères ou d'aiguilles dispersées dans la couche d'additif extérieure du revêtement.
- 45 6. Revêtement selon l'une des revendications précédentes dans lequel les particules aciculaires de la seconde phase comprenant du siliciure d'hafnium sont présentes à la surface externe du revêtement.
- 50 7. Procédé de revêtement à barrière thermique comprenant un substrat en super-alliage à base de cobalt ou de nickel, un revêtement par diffusion de platine-aluminure croissant extérieurement, déposé par dépôt en phase vapeur, sur le substrat en super-alliage à base de cobalt ou de nickel, dans lequel le revêtement par diffusion de platine-aluminure a une microstructure comprenant une zone de diffusion intérieure, adjacente au substrat, et une couche d'additif extérieure, ladite couche extérieure se composant essentiellement de platine, d'aluminium, de nickel, de silicium et d'hafnium, **caractérisé en ce que** le silicium est présent en une concentration comprise entre 55 0,01 % en poids et 8 % en poids, **en ce que** l'hafnium est présent en une concentration comprise entre 0,01 % en poids et 8 % en poids, **en ce que** ladite couche d'additif extérieure comprend une matrice à phase unique comportant des particules dispersées dans celle-ci, formant une seconde phase, **en ce que** lesdites particules de la seconde phase comprennent des siliciures d'hafnium et **en ce que** ledit système de revêtement comprend une couche de céramique sur le revêtement par diffusion d'aluminure.
8. Procédé de revêtement selon la revendication 7 dans lequel le revêtement comprend entre environ 0,01 % et moins de 2 % en poids de silicium, d'hafnium et d'au moins un élément qui est du zirkonium ou un élément actif sélectionné dans le groupe consistant en Ce, La, Y, Mg et Ca dans la couche d'additif extérieure.

9. Procédé de revêtement selon la revendication 7 ou 8 dans lequel le revêtement par diffusion d'aluminure comprend un rapport Hf/Si inférieur à environ 1.
10. Procédé de revêtement selon la revendication 7 ou 8 dans lequel le revêtement par diffusion d'aluminure comprend un rapport Hf + Zr/Si inférieur à environ 1.
11. Procédé de revêtement selon l'une quelconque des revendications 7 à 10 dans lequel les particules aciculaires de la seconde phase en siliciure d'hafnium sont présentes à la surface externe du revêtement.

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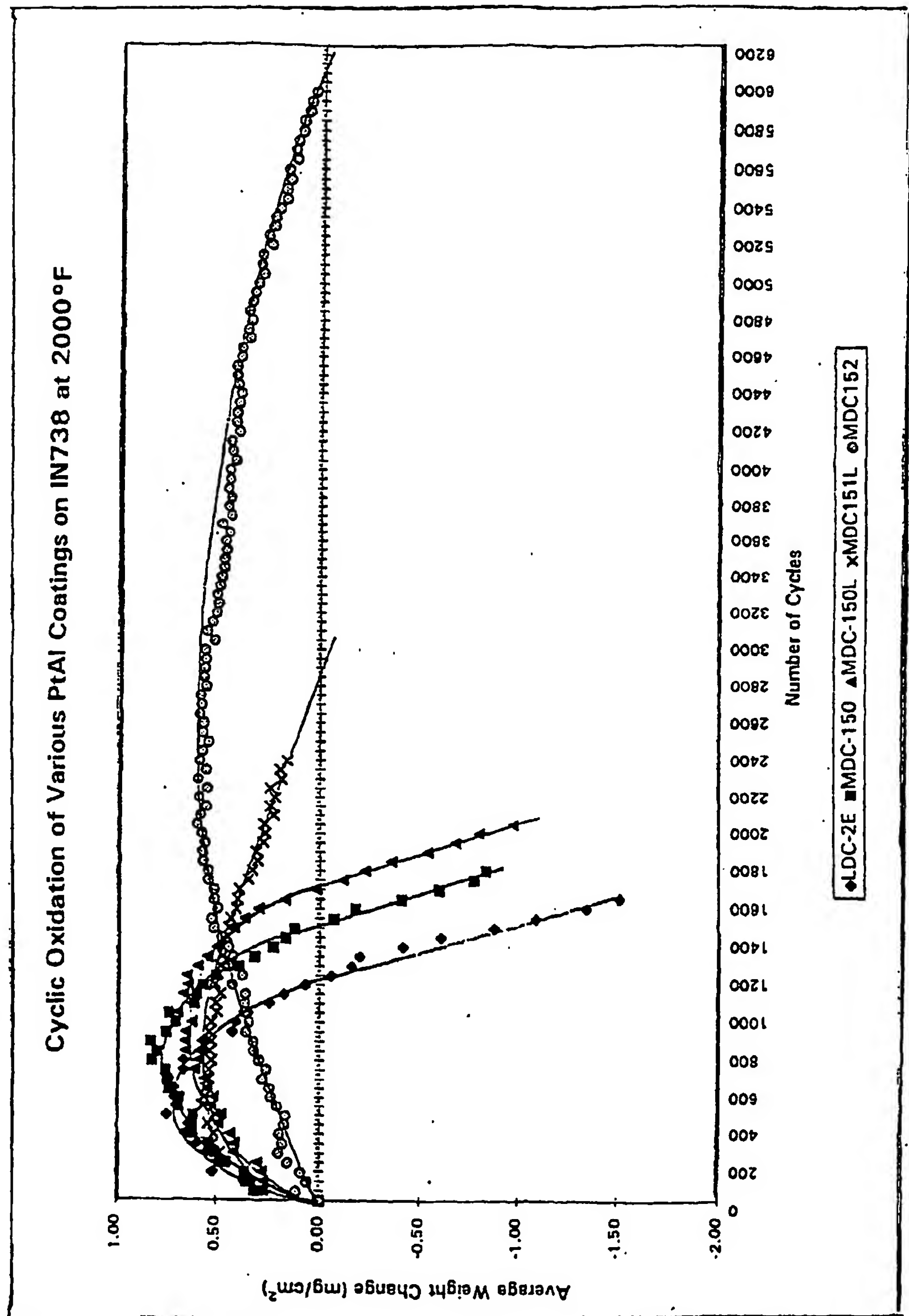


FIGURE 1

2150°F Cyclic Oxidation

Active Element Modified Single Phase Platinum Aluminide Coatings

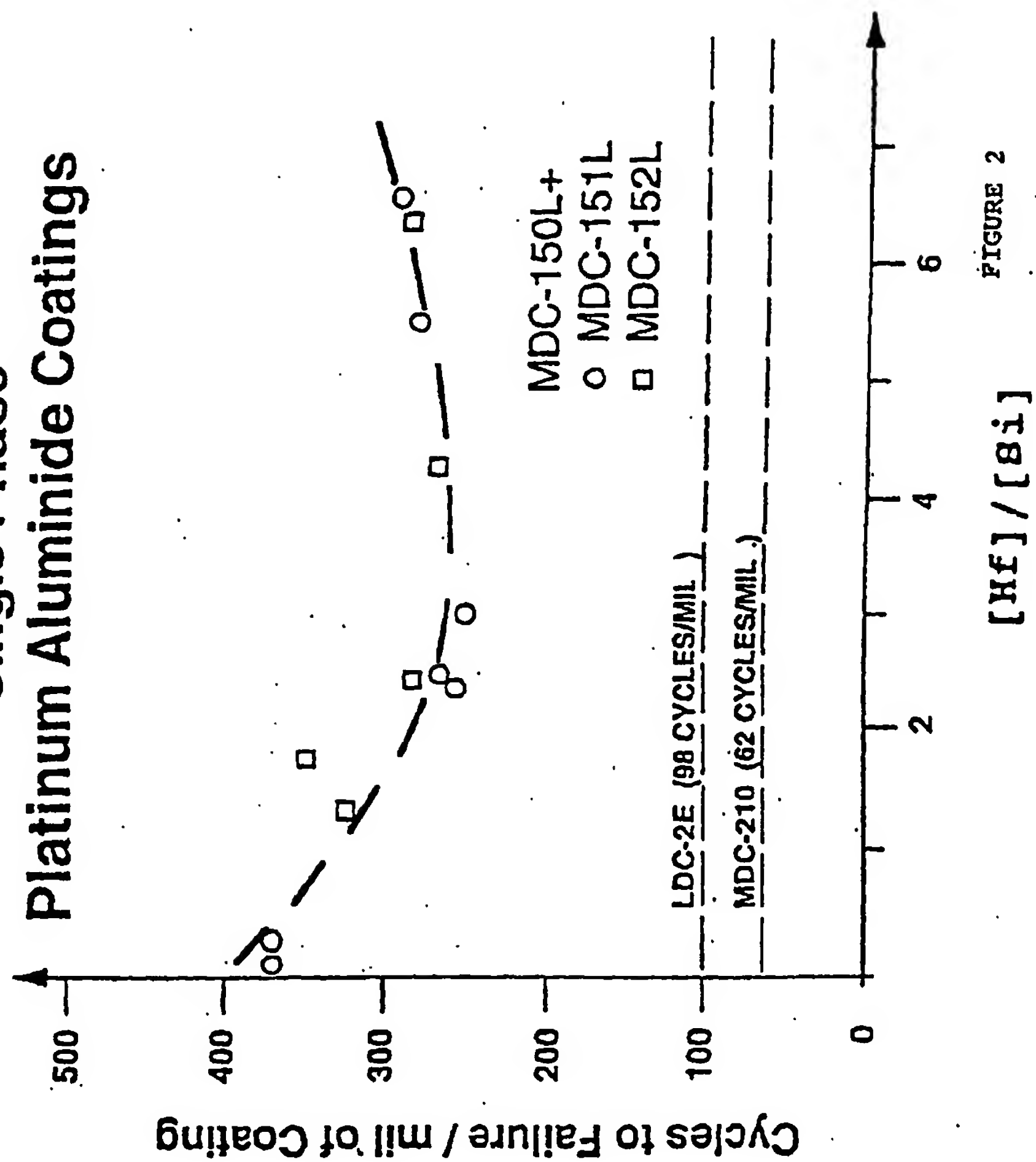


FIGURE 2

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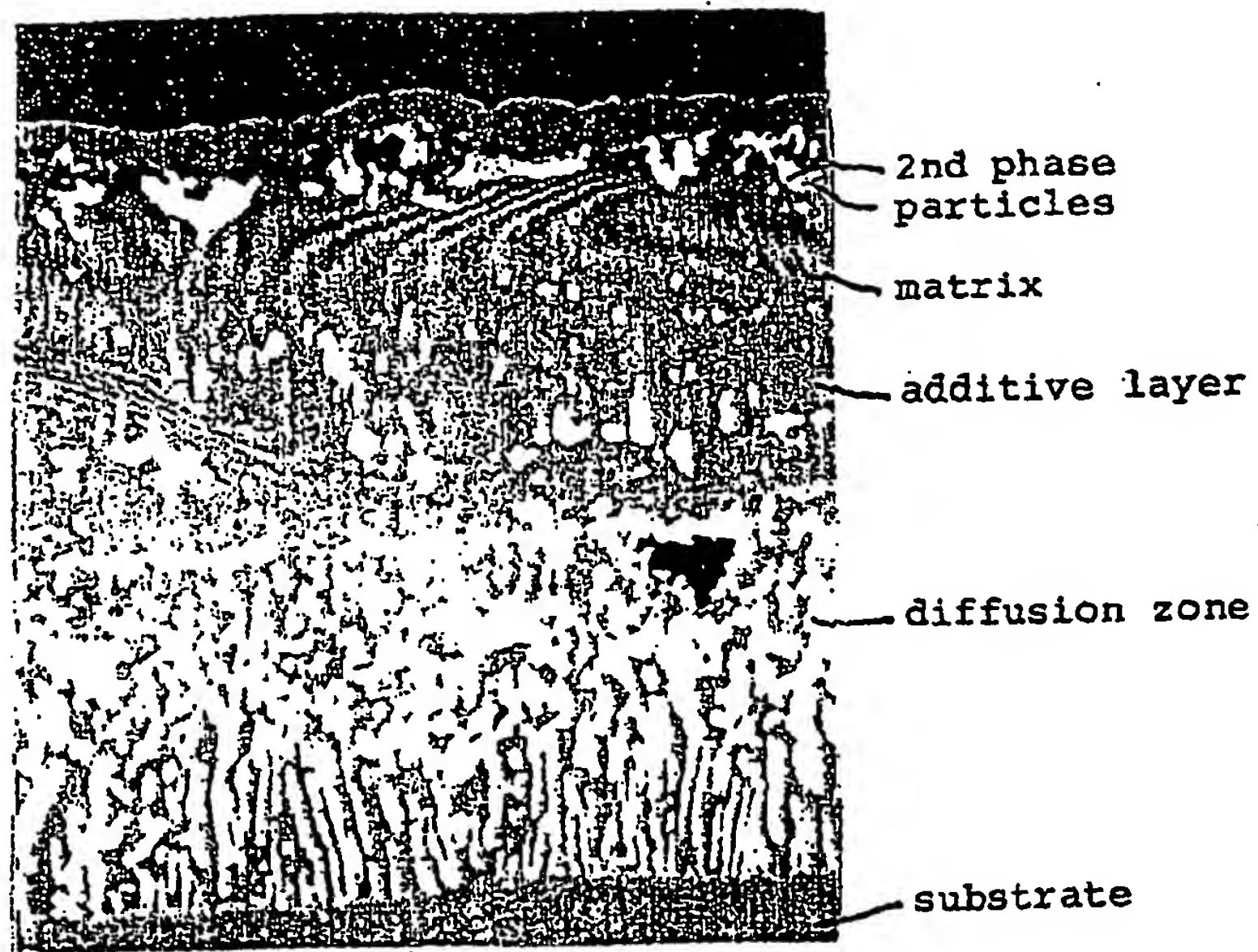


FIGURE 3A

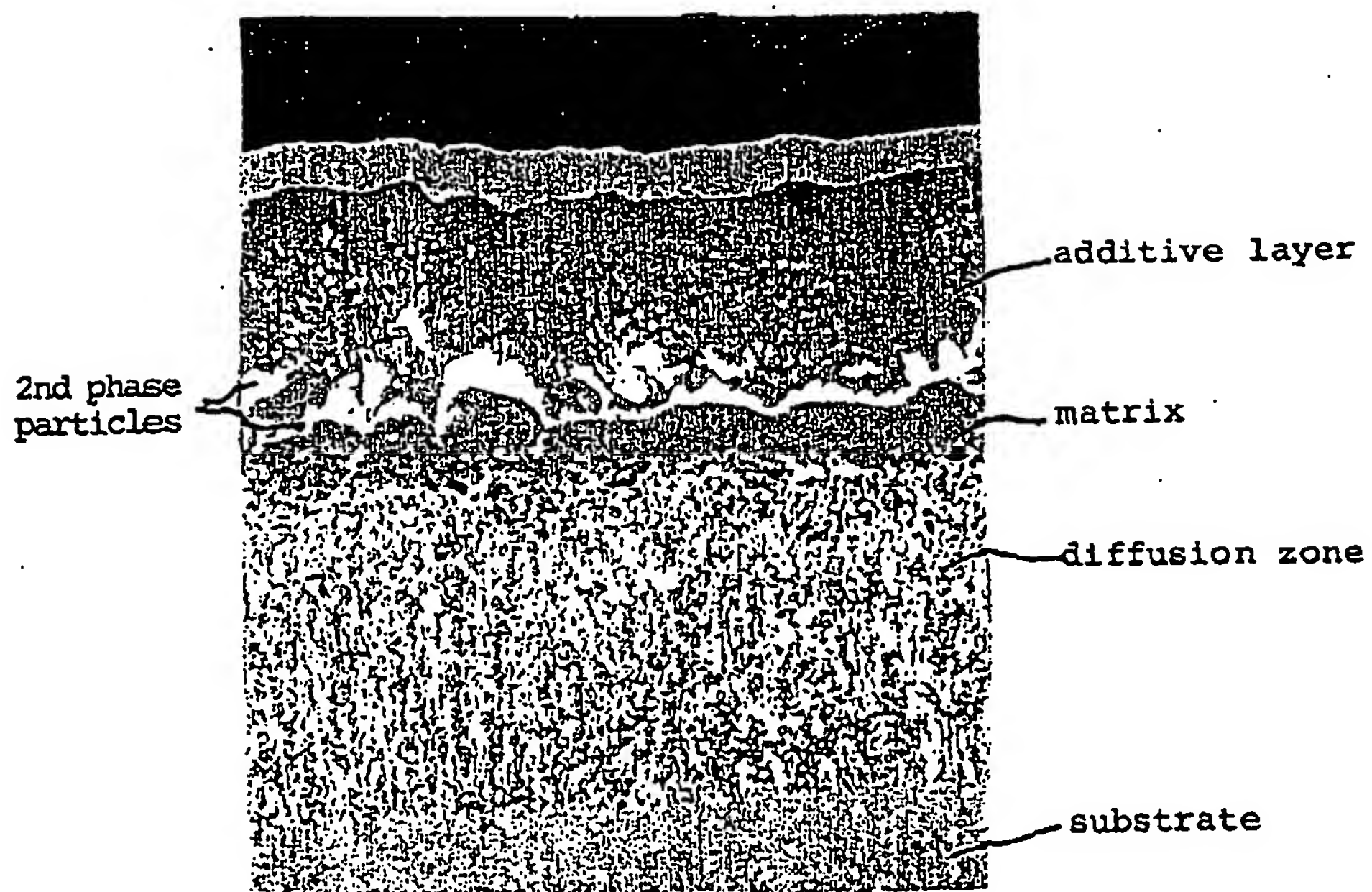


FIGURE 3B

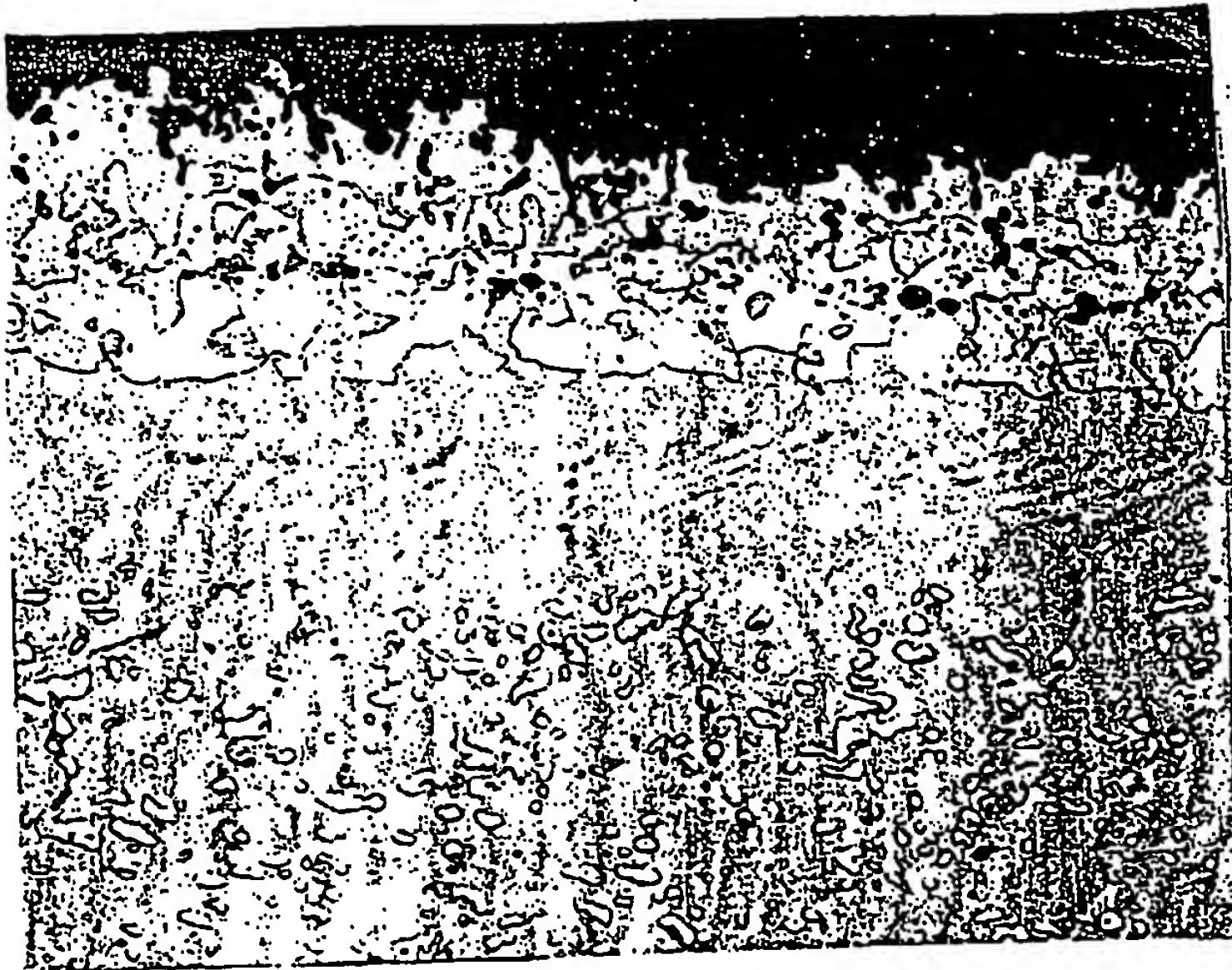


FIGURE 4

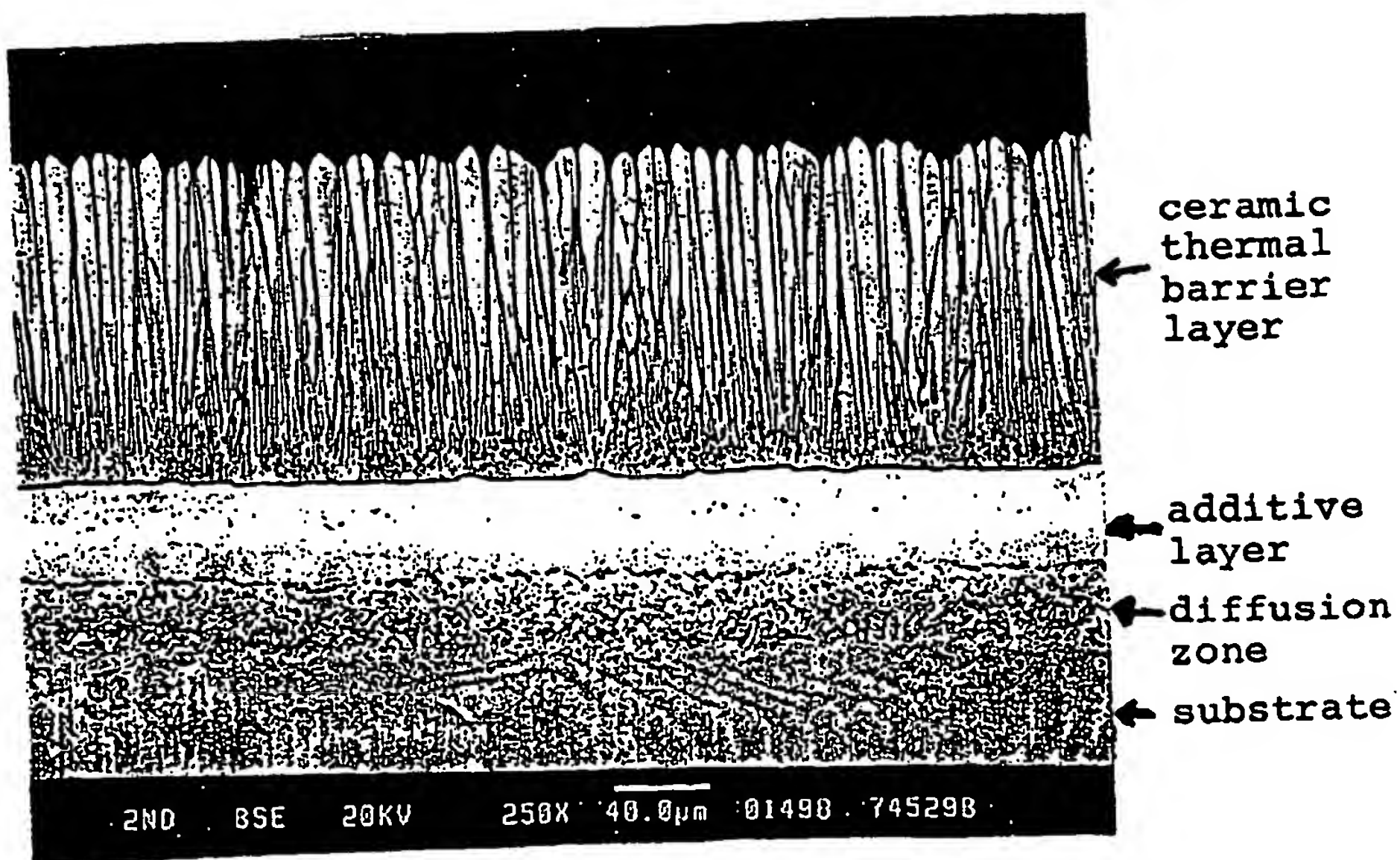


FIGURE 5